

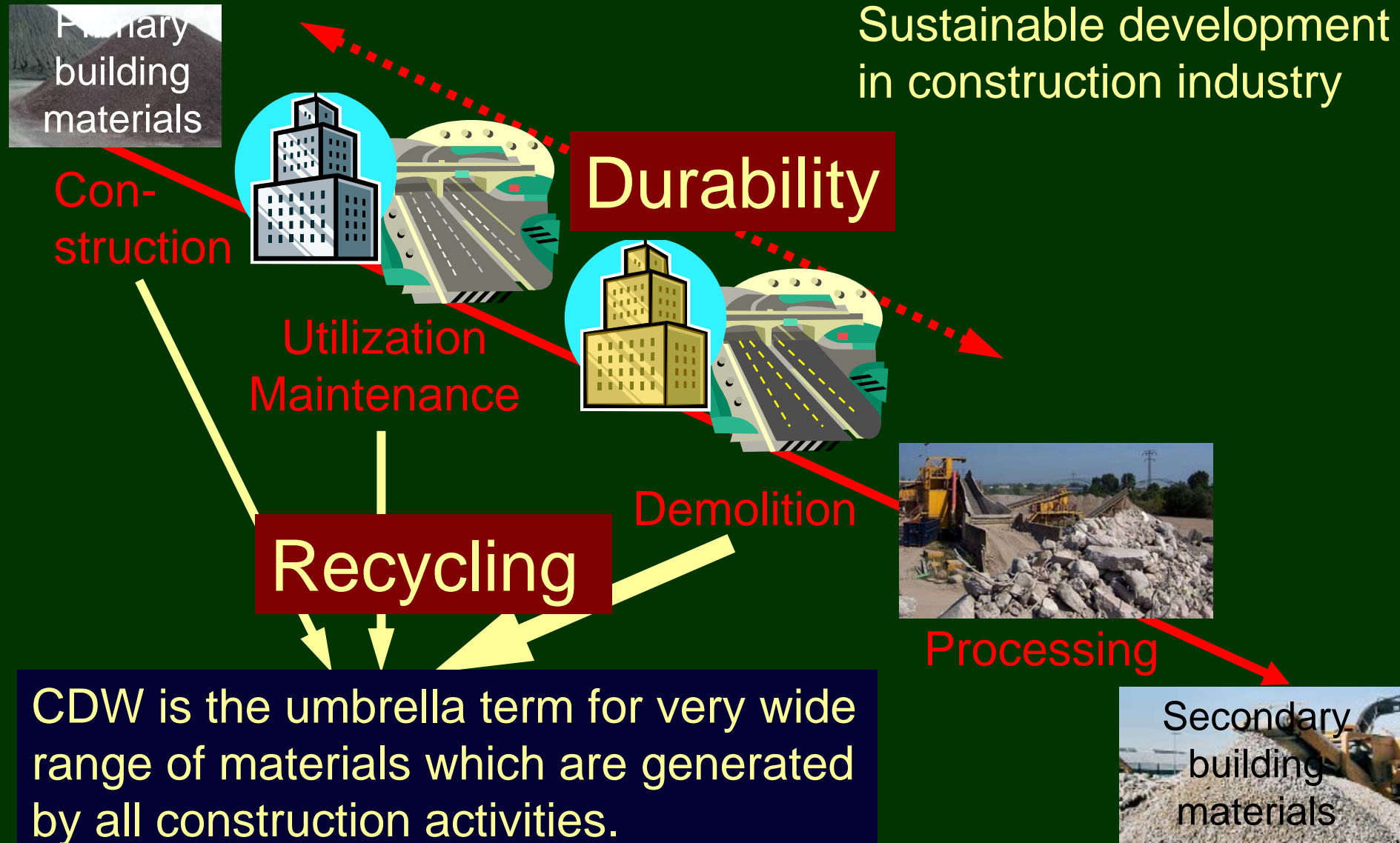
Recycling of construction and demolition waste – Status and new utilisation methods

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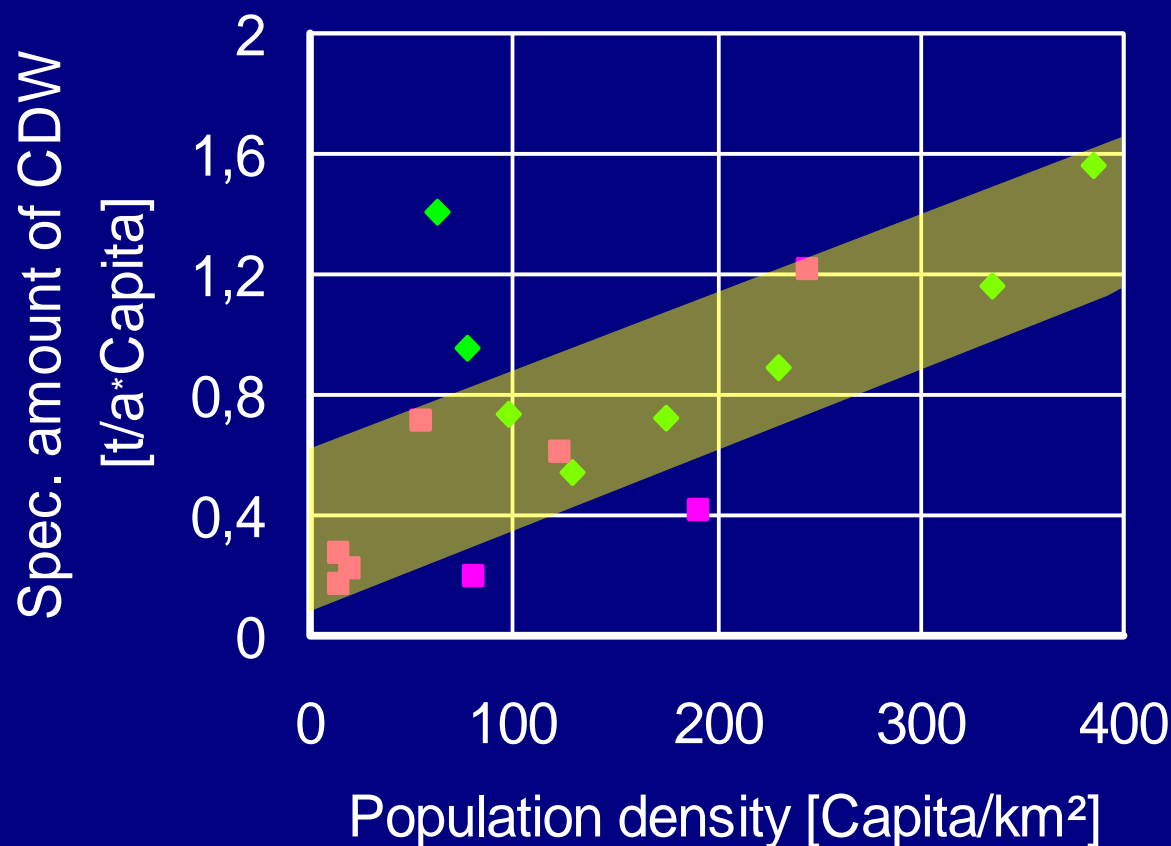
- 1 Sustainable development in construction industry
- 2 Classification and properties of recycled construction materials from CDW
- 3 Closed loop of materials from concrete CDW
- 4 Utilization of masonry CDW as raw material
- 5 Summary and prospects

Sustainable development in construction industry

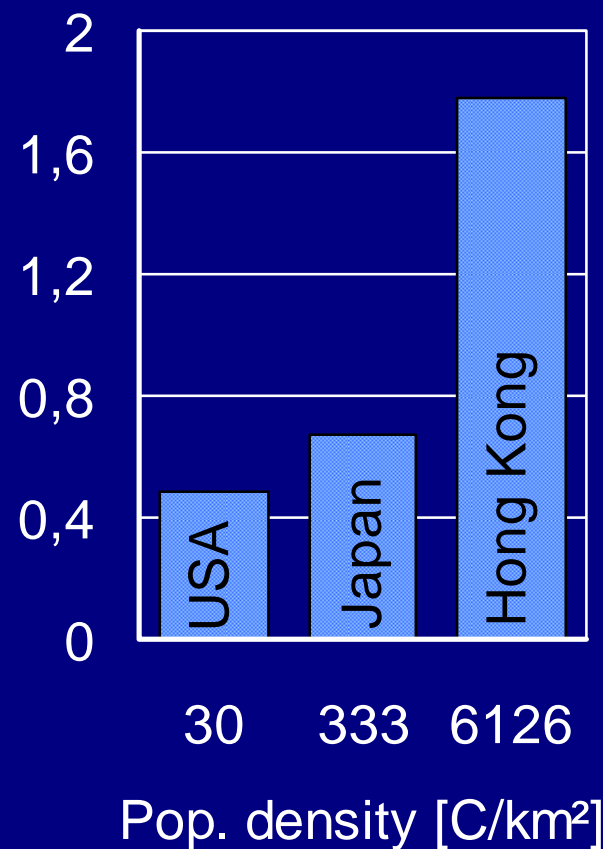


Amount of CDW per inhabitant in Europe

European countries



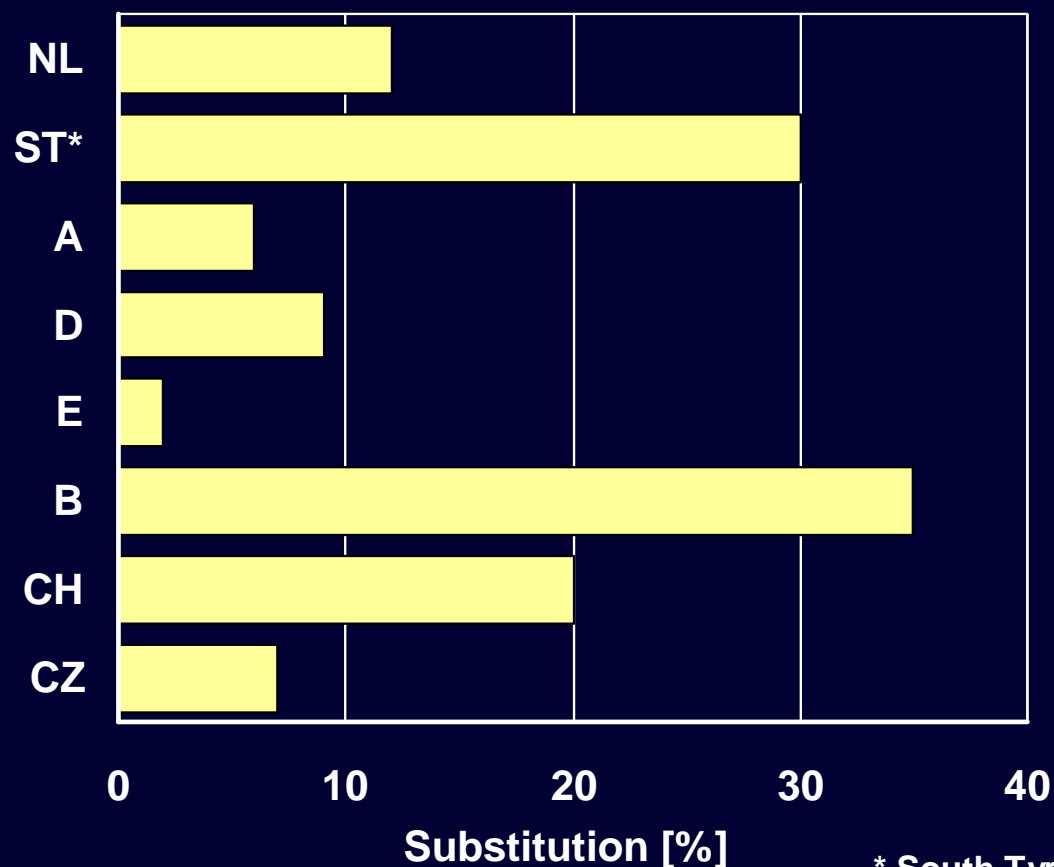
Others



Composition of CDW in Europe

Concrete	2...39 %
Asphalt	6...21 %
Masonry CDW	42...92 %
Mixed rubble	2...11 %

Substitution of natural materials by recycled materials



* South Tyrol

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Features for classification

Composition

Division in at least three main groups

- Concrete + mortar + natural aggregates
- All kinds of brick + ceramics
- Asphalt

Bulk density (water absorption)

Division in at least two groups

- $> 2,0$ (OD) / $2,2$ (SSD) kg/m^3
- $> 1,5$ (OD) / $1,8$ (SSD) kg/m^3

Content of leach- able substances

Division in at least two groups

- Material without contaminations
- Material with contaminations lower than certain, defined threshold values

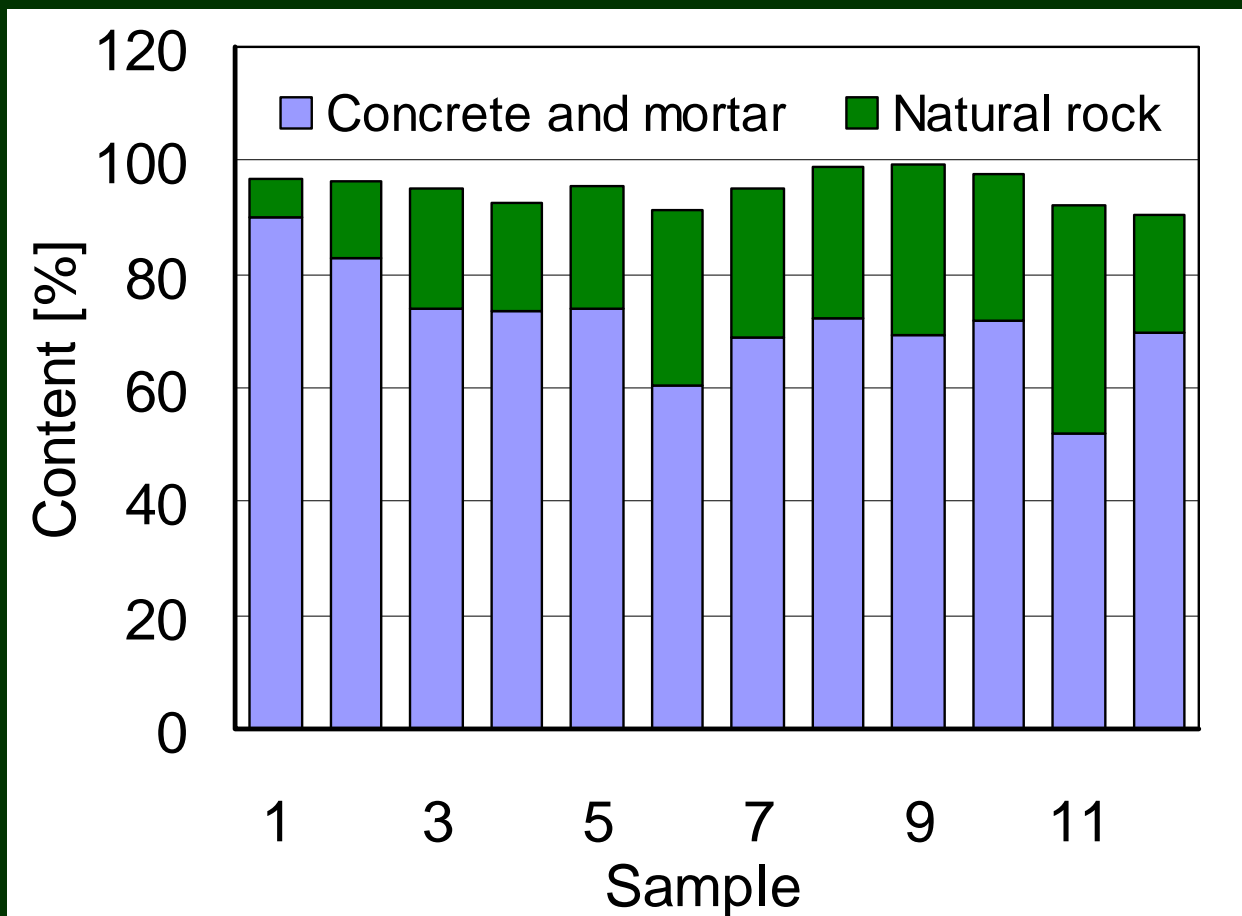
German standard on recycled aggregates DIN 4226-100

Constituents [% by mass]	Type 1	Type 2	Type 3	Type 4
DIN 4226-100: Recycled aggregates	Concrete chippings + crusher sand	Construction chippings + c. sand	Masonry chippings + c. sand	Mixed chippings + c. sand
Concrete and natural aggregates	≥ 90	≥ 70	≤ 20	≥ 80
Clinker, non-pored bricks	≤ 10	≤ 30	≥ 80	
Sand-lime bricks			≤ 5	
Other mineral materials (i.e. pored brick, lightweight concrete, no-fines concrete, plaster, mortar, porous slag, pumice stone)	≤ 2	≤ 3	≤ 5	≤ 20
Asphalt	≤ 1	≤ 1	≤ 1	
Foreign substances (i.e. glass, non ferrous metal slag, lump gypsum, plastic, metal, wood, plant residue, paper, others)	≤ 0.2	≤ 0.5	≤ 0.5	≤ 1
OD density/oven dry [kg/m^3]	≥ 2000	≥ 2000	≥ 1800	≥ 1500

Ref.: DIN 4226-100

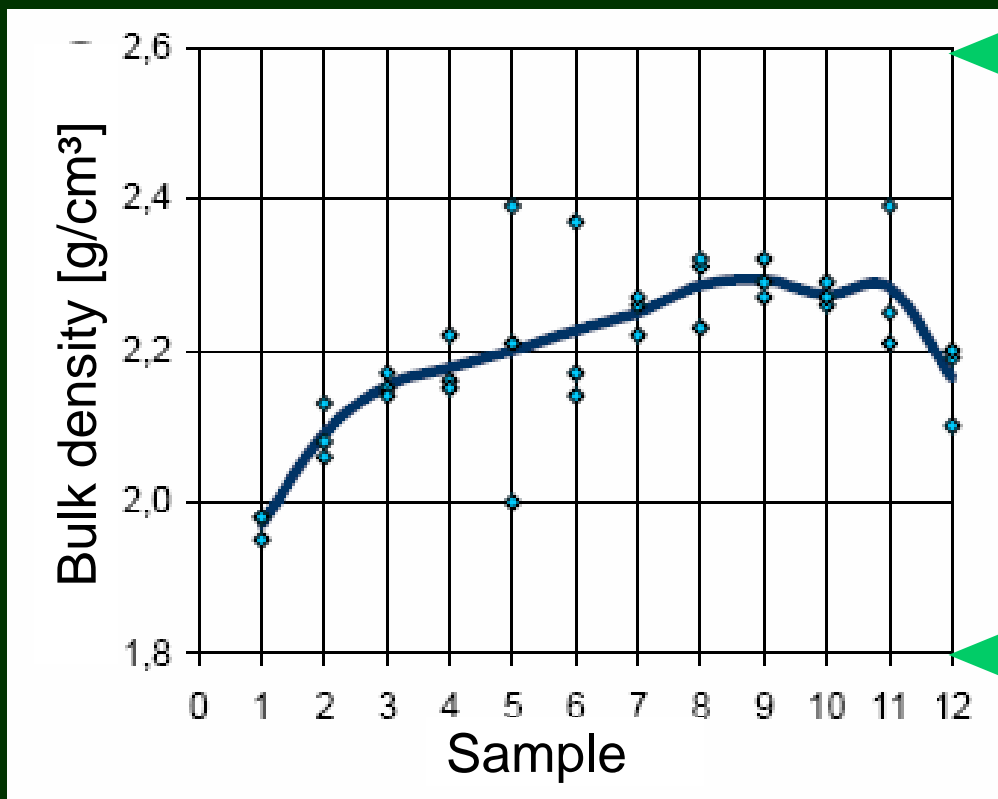
Properties of real concrete CDW

Composition of processed concrete from one recycling plant



Mean: 95.1 %
 Variation
 coefficient: 3.1 %

Bulk density of processed concrete from one recycling plant

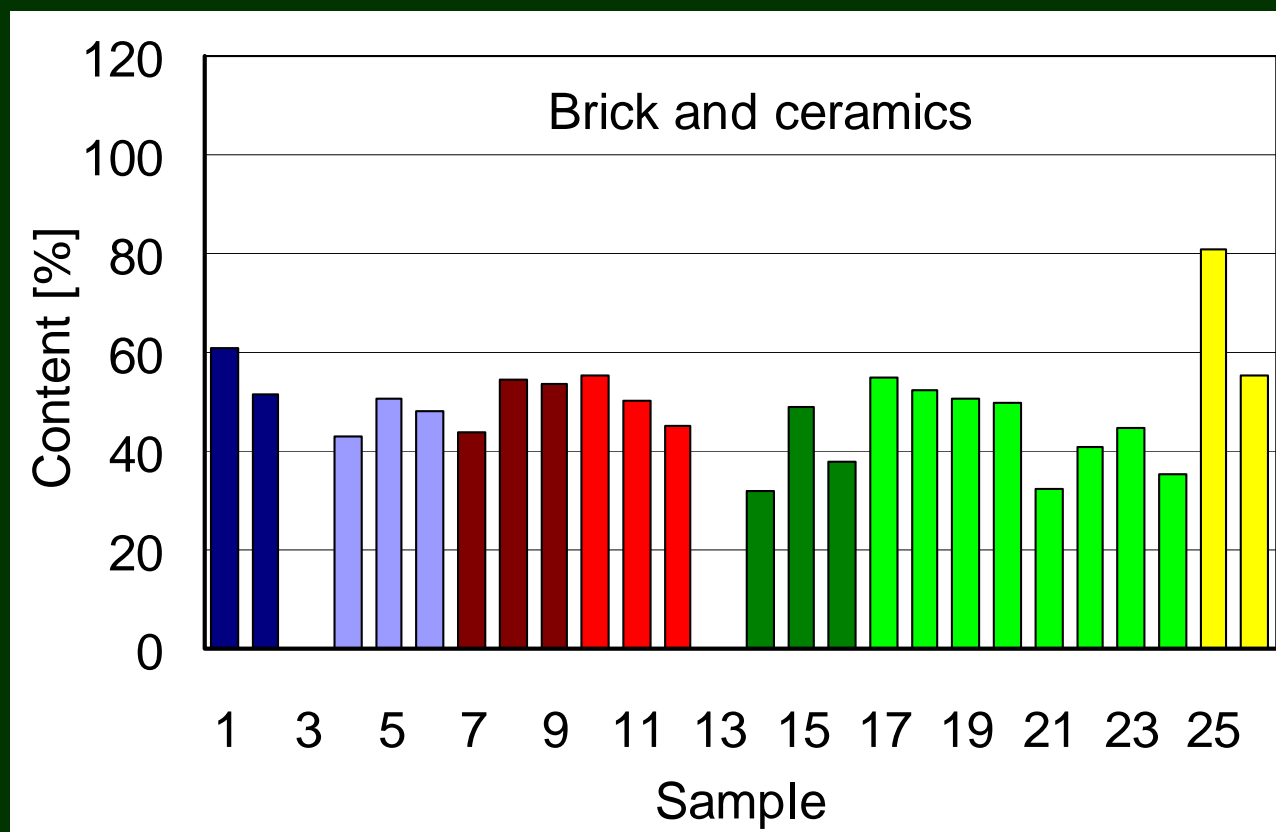


Nat. aggregate

Mean: 2.20 g/cm³
Variation
coefficient: 4.4 %

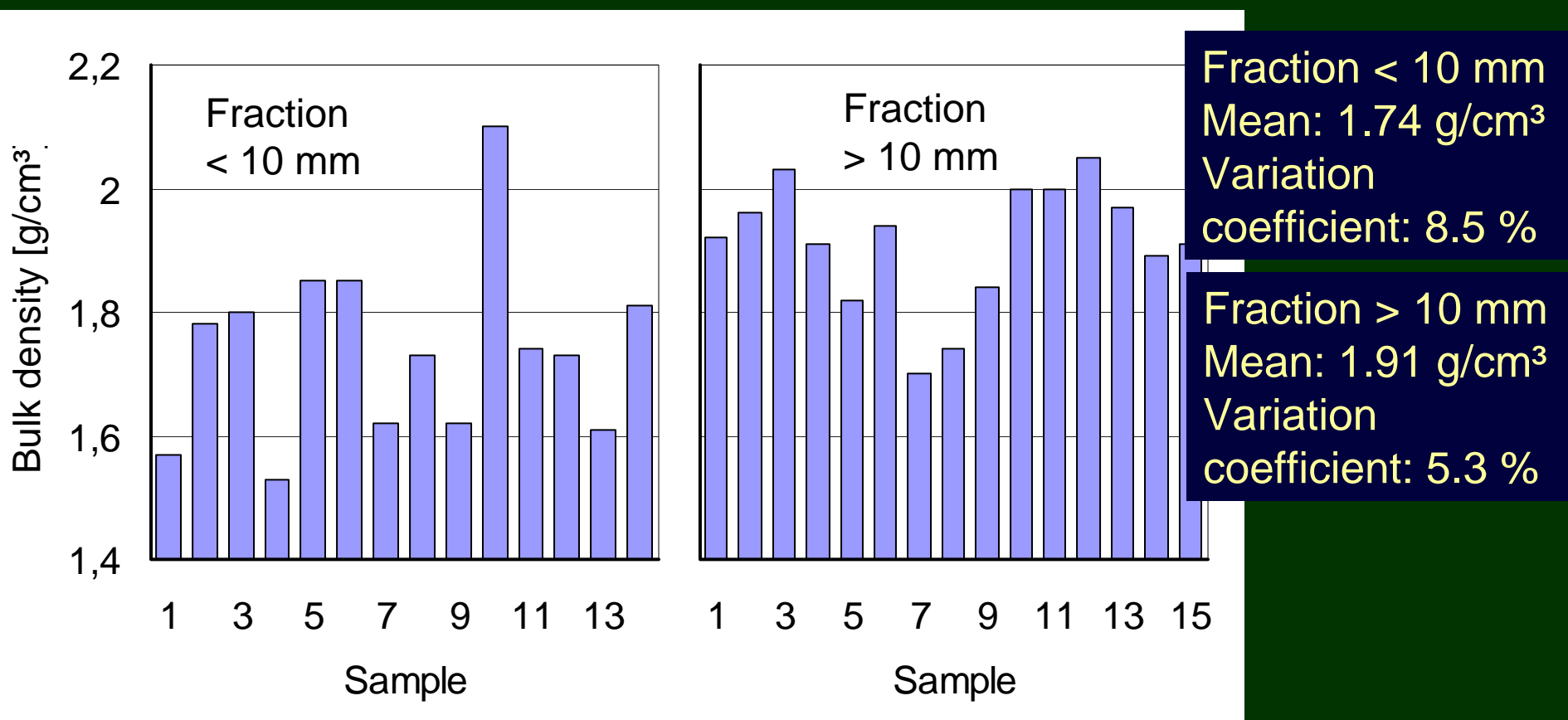
Cement paste

Composition of processed masonry from several recycling plants



Mean: 48.3 %
Variation
coefficient: 21.3 %

Bulk density of processed masonry from several recycling plants



Conclusion: Considerable fluctuations in composition and density

Concrete CDW: Caused by composite nature of concrete more than by composition

Masonry CDW: Caused by composition

Consequences for reuse in closed loops

High-grade applications not realizable so far due to unstable quality of processed CDW

Technologies for quality improvement and homogenization have to be developed

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Coarse recycled concrete aggregates: Composites of cement paste and natural aggregate

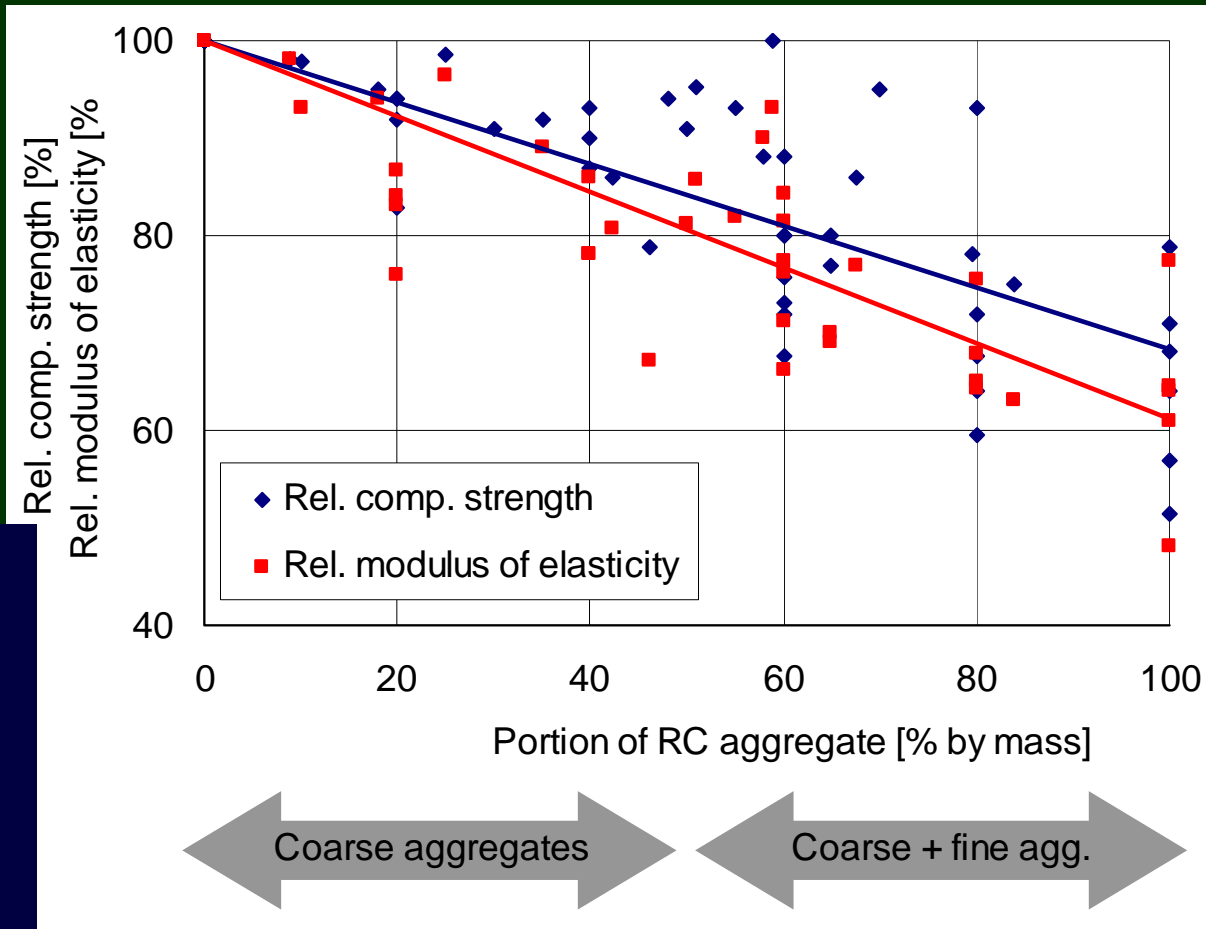


Consequences of the composite nature on properties of secondary concretes

- ⇒ Fresh concrete: Increase of water absorption and loss of workability caused by additional porosity of the adhered cement paste
- ⇒ Hardened concrete: Loss of compressive strength caused by increased porosity.
- ⇒ Hardened concrete: Loss of modulus of elasticity as a result of higher porosity and higher content of CSH phases.
- ⇒ Further effects on shrinkage, creep and durability.

Mechanical properties vs. portion of recycled aggregates

Replacement of coarse
and fine aggregates
 Δ Strength \rightarrow 32 %
 Δ E-modulus \rightarrow 39 %
Replacement of coarse
aggregates only
 Δ Strength \rightarrow 16 %
 Δ E-modulus \rightarrow 20 %

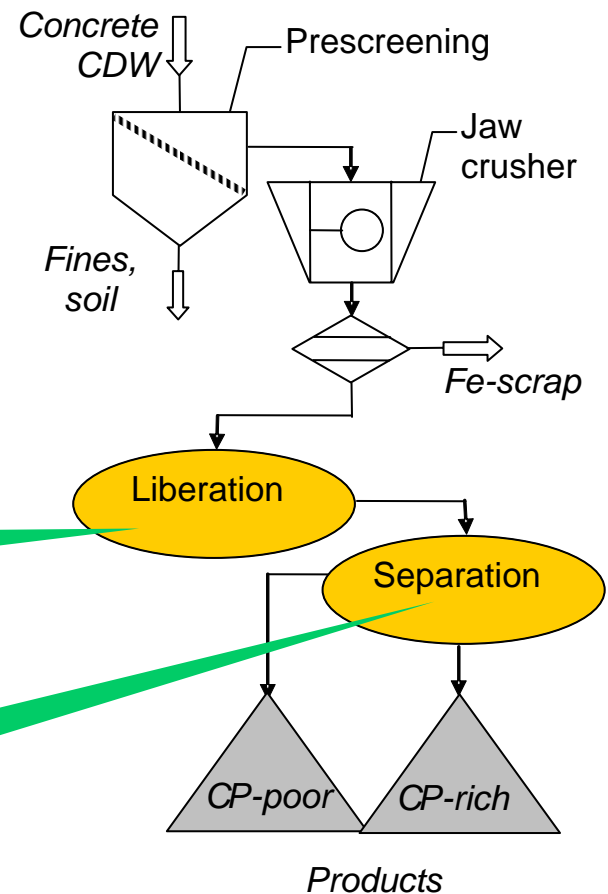


Consequences for quality improvement of coarse recycled aggregates

Generation of cement paste free aggregates with suitable techniques for liberation and separation

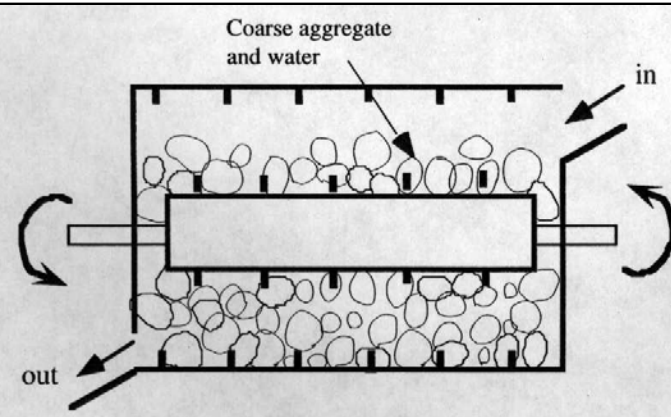
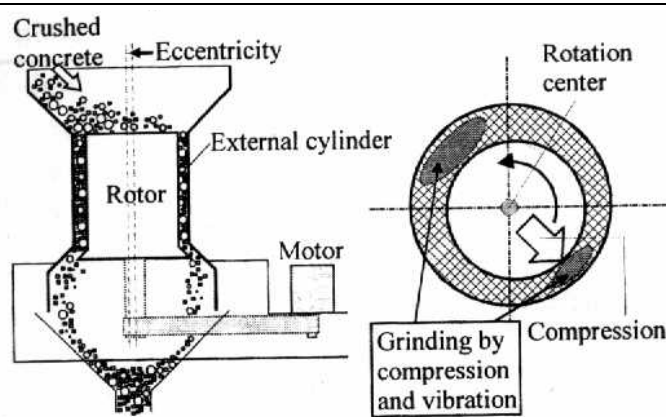
Mechanical or thermal liberation

Separation by particle size or density

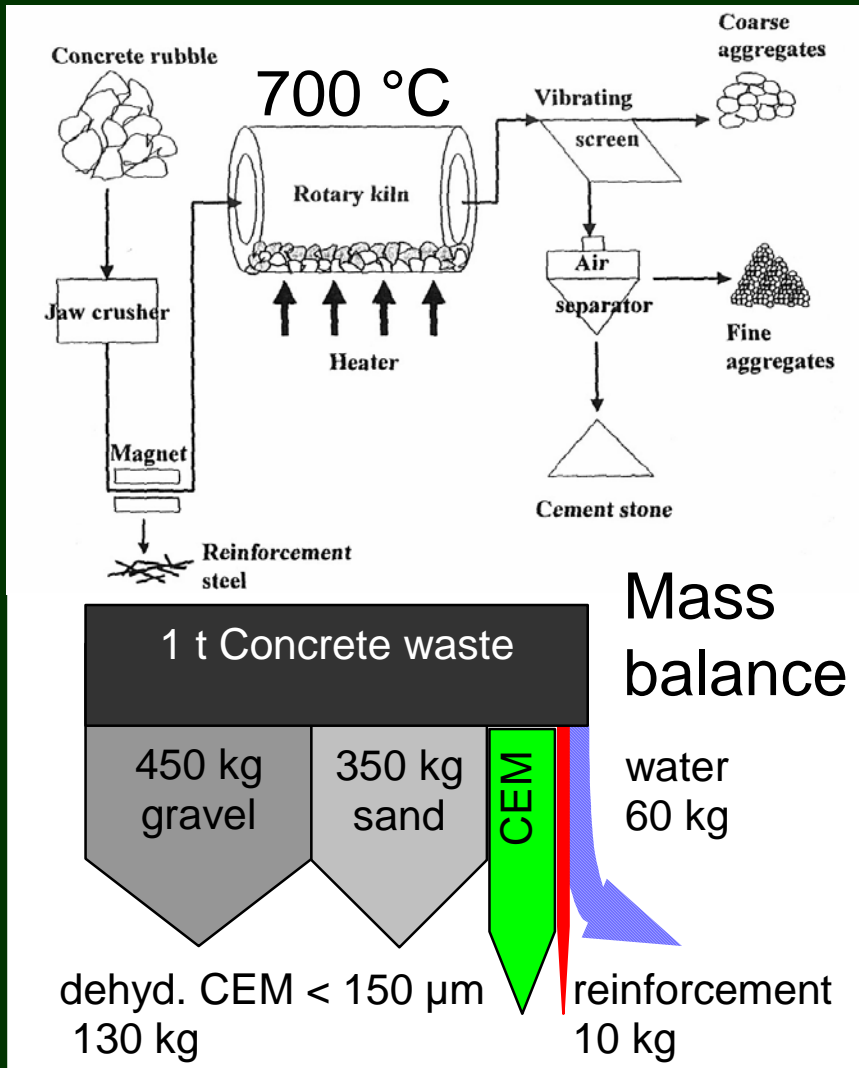


Removal of adhering cement paste by abrasion stress

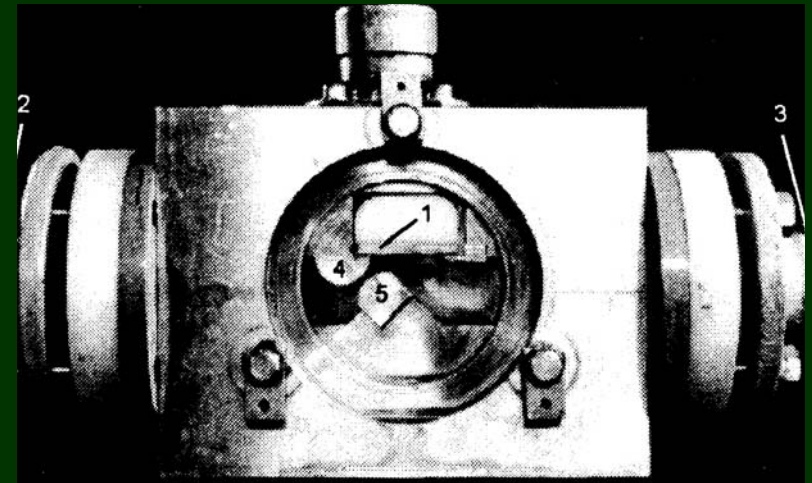
External cylinder: Ø 720 mm; height 800 mm
Rotor: Ø 720 mm; height 800 mm; 500 U/min
Eccentricity: 11.7 mm

Reference	Kasai [1993]	Yanagibashi [2002]
Operating mode		
Material parameter		
Virgin aggregates	$\rho = 2.62 \text{ g/cm}^3$ $WA \rightarrow 0$	$\rho = 2.5...2.61 \text{ g/cm}^3$ $WA = 1.2...3.6 \%$
Secondary aggregates	$\rho = 2.52 \text{ g/cm}^3$ $WA = 3.0 \%$	$\rho = 2.4...2.53 \text{ g/cm}^3$ $WA = 1.8...5.4 \%$

Applying of thermal stress



Applying of cavitation stress



Flow cavitation chamber
with specimen (1)

Degree of separation
between 46 und 90 %

Applying of high performance sonic impulses (HPSI)

Electrical energy

Disruptive electrical
discharge under water

Shock wave

- Pressure amplitudes up to 100 MPa
- Rise time $< 5 \mu\text{s}$

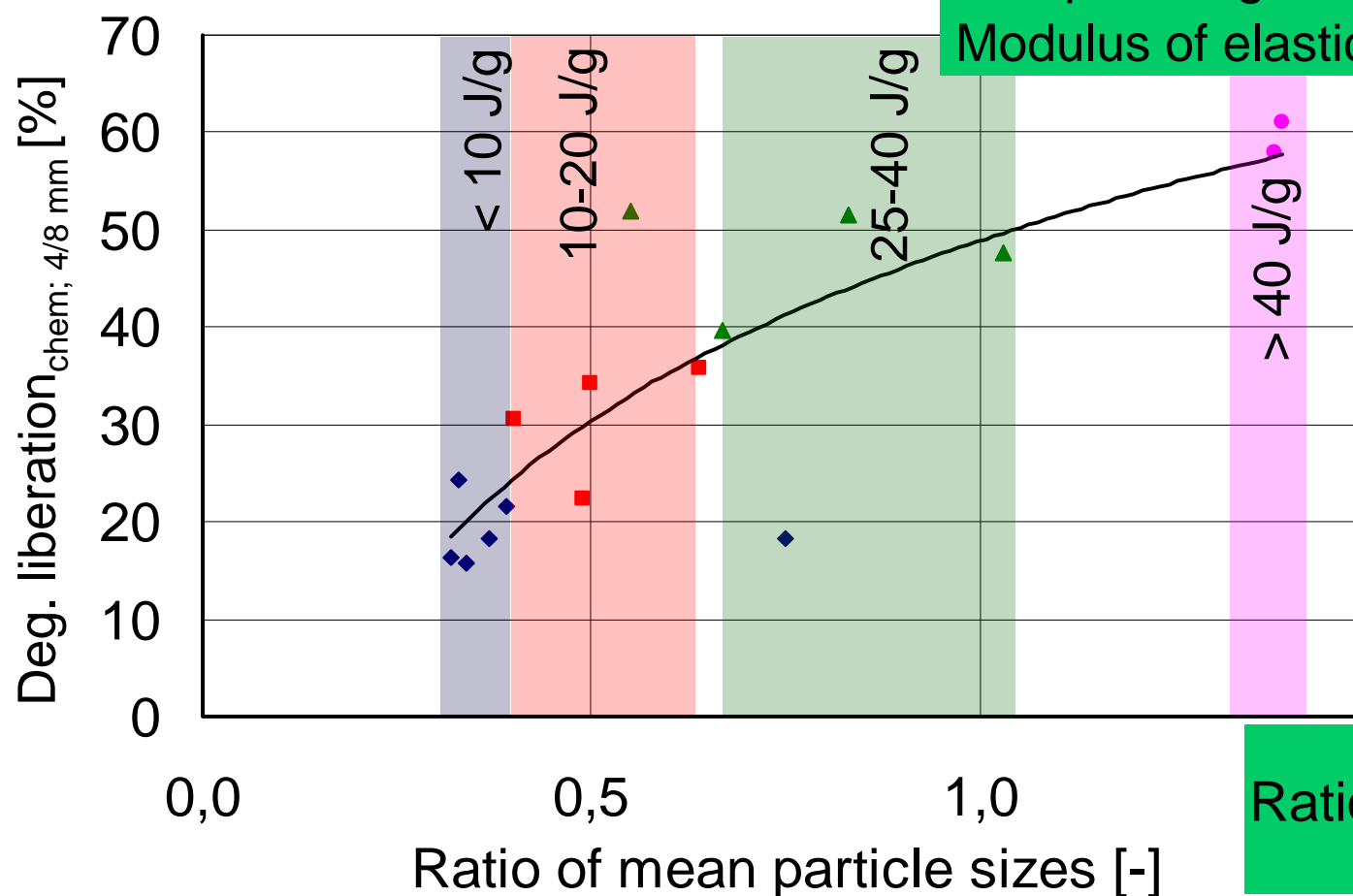
Reflexions at interfaces
of different density

Generation of pressure
and tensile stresses

Failure at the interfaces



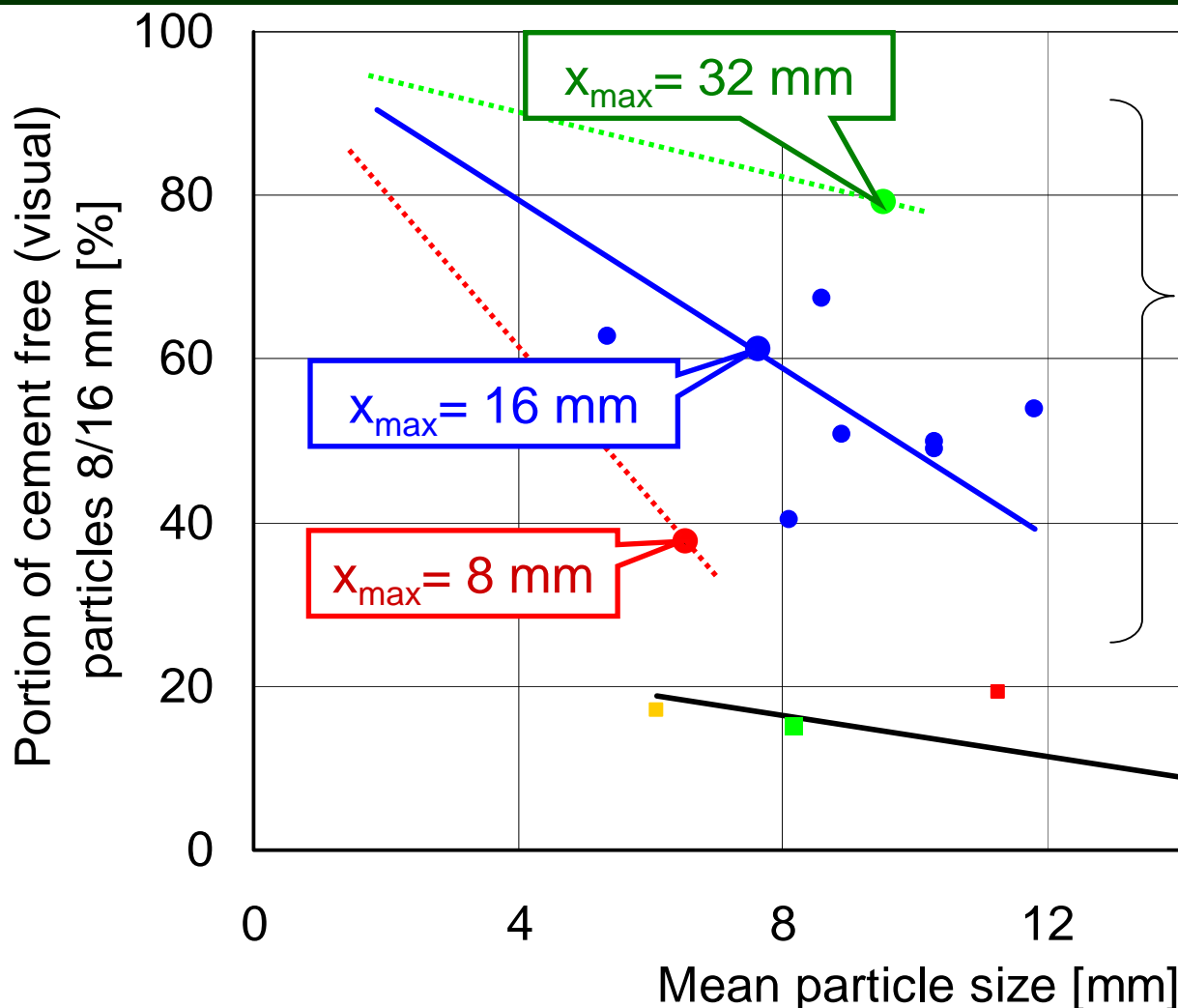
Degree of liberation versus ratio of size reduction



Concrete B 25: 300 kg/m³ CEM I
 32,5 R + 180 kg/m³ water + 1902
 kg/m³ quartz sand and gravel AB 16
 Comp. strength: 36 N/mm²
 Modulus of elasticity: 33 kN/mm²

$$\text{Ratio} = \frac{x_{m, \text{original aggregate}}}{x_{m, \text{crushed product}}}$$

Degree of liberation after treatment in impact crusher or by HPSI



Concrete B 25 with
varying maximum particle
size of aggregates: 8 mm;
16 mm; 32 mm.

Specific energy
consumption

HPSI

⇒ 0.05 MJ/kg for
comminution of concrete
⇒ 0.08 MJ/kg for
comminution + liberation

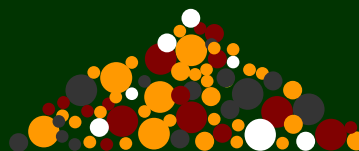
Impact
crusher

⇒ 0.01 to 0.02 MJ/kg
for comminution

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Expanded granulates from masonry rubble

Masonry CDW as mixture of different materials



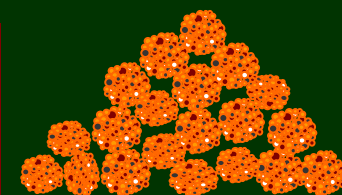
Crushing and grinding

Addition of SiC as expanding agent

Mixing and shapening

Thermal treatment

Lightweight
aggregate



Raw materials

Masonry CDW 0/4 mm from a
recycling plant as matrix material

SiO ₂	Al ₂ O ₃	FM
[%]		
63,1	17,7	19,1

Aerated autoclaved concrete from AAC
plant as additional material to increase
the heterogeneity

SiO ₂	Al ₂ O ₃	FM
[%]		
53,0	4,4	42,6

Silicium carbid waste < 100 µm as expanding component

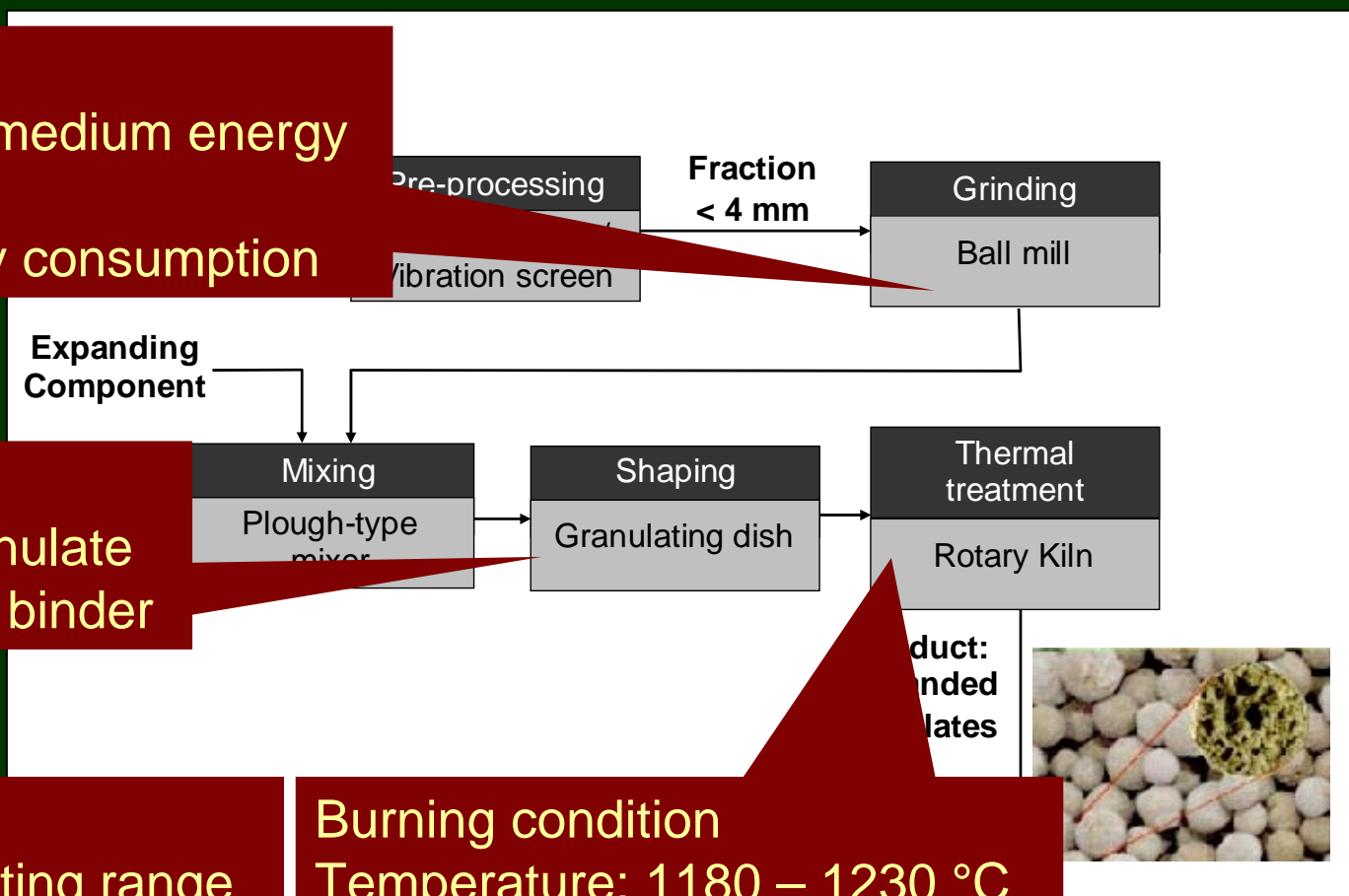
Manufacturing process

Grindability
Masonry CDW – medium energy consumption
AAC – low energy consumption

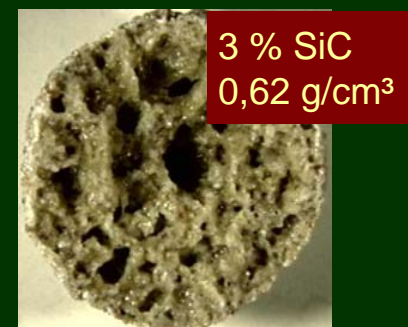
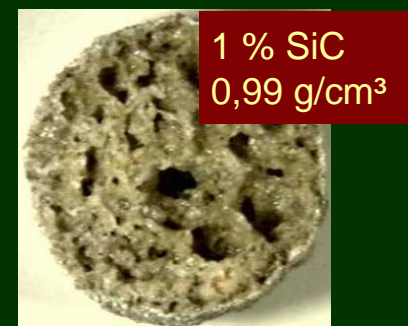
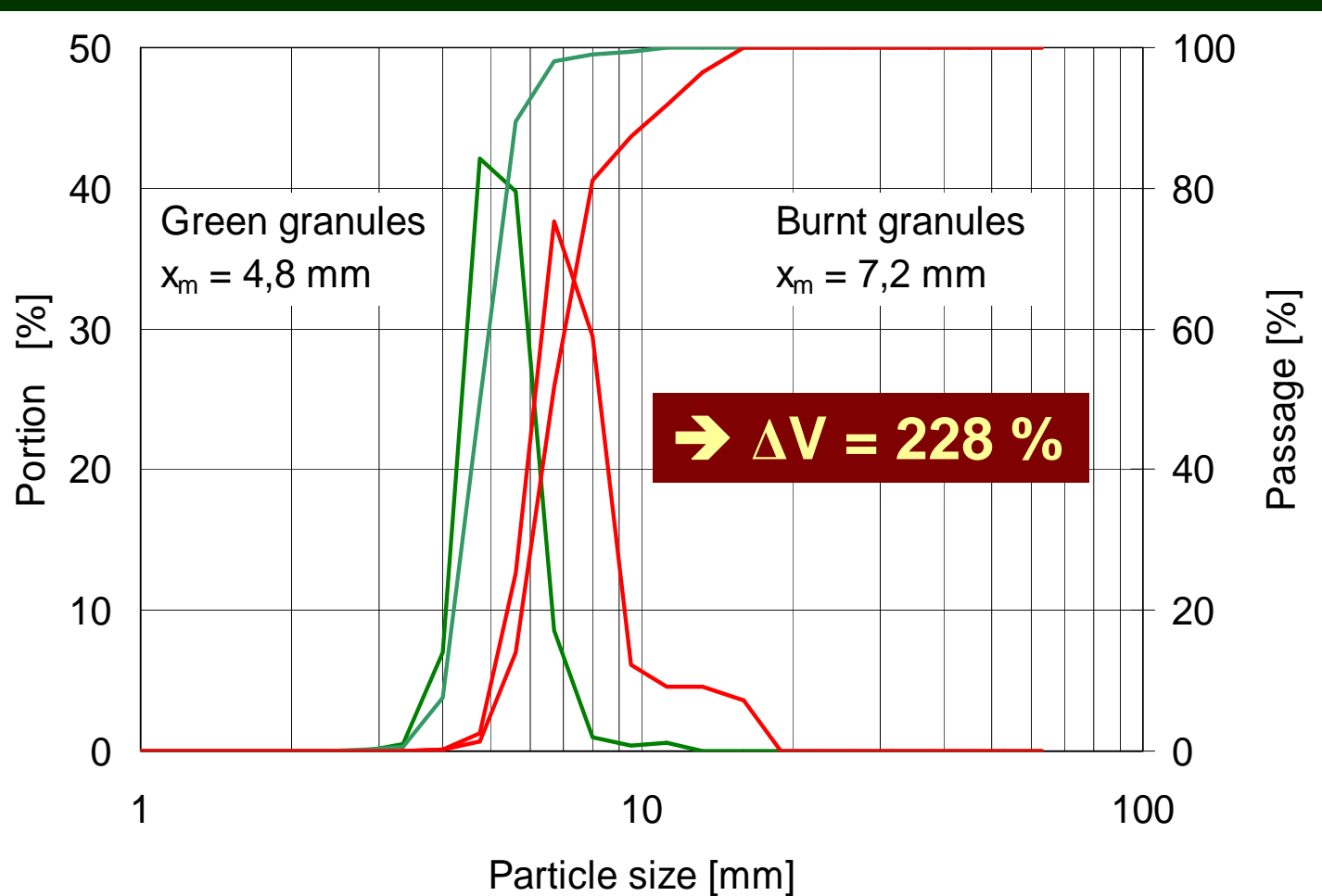
Shaping
Easily able to granulate without additional binder

Influence of AAC
Shortening of melting range
Max. content of AAC: 50 %

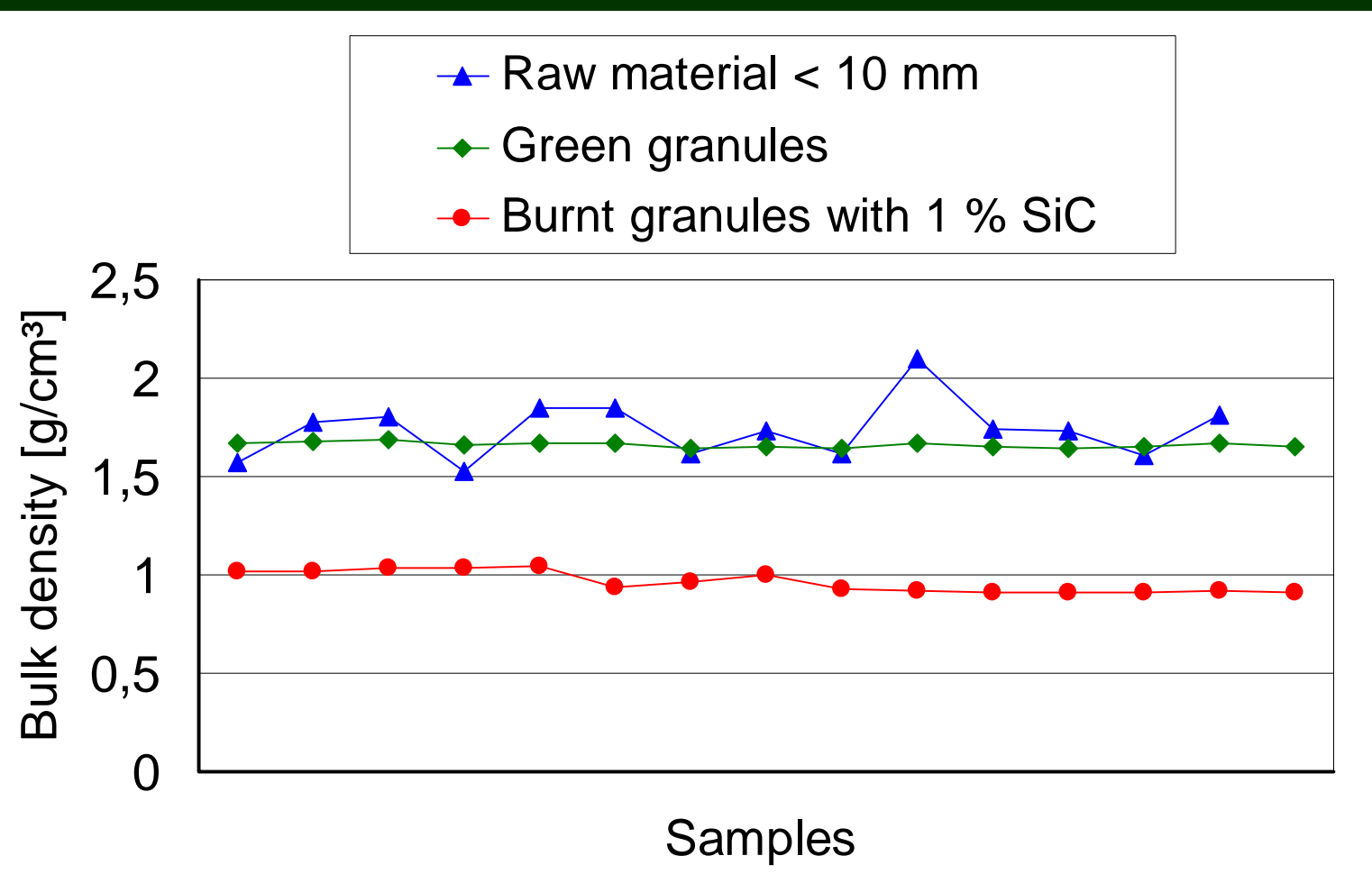
Burning condition
Temperature: 1180 – 1230 °C
Residence time: about 20 min



Expanding process during the thermal treatment



Effect of the processing on homogeneity



First application tests

- Manufacturing of blocs and cubes in a precast concrete plant
- Volumetric substitution of the normally used expanded clay 4/8 mm by CDW aggregate 4/8 mm



	CDW aggregate	Expanded clay
Bulk density of concrete [kg/m ³]	1130	870
Com. strength [N/mm ²]	11,90	6,16
Thermal conductivity [W/mK]	0,35	0,24
Freeze-thaw resistance: E _{dyn} change [%]	- 2,6	- 67,9

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Summary

1. Construction and Demolition Waste is characterized by rather large variation range of the composition as well as the physical properties.
2. Main field of application of CDW: Unbounded systems like fills and embankments.
3. Reuse of concrete CDW as secondary aggregates requires incorporation of liberation techniques into the processing.
4. As advanced liberation technique the treatment by high performance sonic impulses results in clear quality improvement.

5. Reuse of masonry CDW in construction requires technologies which improve quality and homogeneity.
6. Own experiments show feasibility of masonry CDW as raw material for manufacturing of lightweight granulates.
7. Properties of the lightweight granulates are rather constant and at least equal to those of other mineral lightweight materials.

Further research must be aimed at

- ⇒ the scale up of both technologies,
- ⇒ examinations of product quality and uniformity and
- ⇒ comparative studies about the energy demand.

**Thank you for your
attention !**

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